

# Structural Calculations



## Mercer Island High School 80' Communication Tower



**SESEA00387B Mercer Island**  
Atop the Theater Building  
9100 S.E. 42<sup>nd</sup> Street  
Mercer Island, WA 98040  
King County

Sidesway Project No. 21052.05

**Results Summary: Sufficient Capacity**

Prepared By:



02/10/24

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## Project Description

Sidesway Engineering was retained by Day Wireless to analyze the existing 80' communication tower located atop the roof of the high school theater building at 9100 S.E. 42<sup>nd</sup> Street on Mercer Island. Dish Wireless is proposing to add a 2'Ø microwave dish to their recent 2022 panel antenna installation at the top of the tower.

The tower was designed by Rohn and was placed atop the new theater building constructed in 1998. The original tower and building drawings were obtained and the drawings indicated that the building design accounted for the tower with additional framing and details specific to the tower installation. Our analysis was performed based on the information within the original design documents, which included geometry, member sizes, and material strengths.

## Tower Loading

The appurtenance loading utilized in this analysis is summarized in the table below. This represents the antennas that currently exist on the tower and the proposed Dish Wireless equipment. Mount elevations represent the centerline of the mount system relative to grade.

Mount Elev.	Qty	Equipment	Qty	Feedline	Comments
135'	3 3 3 1	Commscope FFV-65A-R2-V1 Panels Samsung RF4450T-71A RRUs Samsung RF4451D-70A RRUs Raycap RDIDC-9181-PF-48	1	1.6"Ø Hybrid	Existing (Dish)
135'	1	Commscope VHLP2-18 MW Dish	1	1/2"	Proposed (Dish)
119'	1	4-Bay Single Dipole on 2' Standoff	1	1/2"	Existing
105'	1	Shively Model 6812B 2-Bay Half Wave FM Antenna	1	1 <sup>5</sup> / <sub>8</sub> "	Existing (M.I.)
77'	1	4-Bay Single Dipole on 2' Standoff	1	1/2"	Existing

## Tower Design Criteria

A rigorous analysis was performed to determine if the tower is compliant with the current design standard, ANSI/TIA-222-H "Structural Standard for Antenna Supporting Structures, Antennas, and Small Wind Turbine Structures." The wind and seismic parameters used in our analysis are listed below. These represent the most stringent requirements of either the local jurisdiction or Annex B in the ANSI/TIA-222-H Standard. The tower is a Class III structure since it is located atop a school.

### Wind Analysis Criteria:

Basic wind speed w/o ice = 105 mph  
Basic wind speed w/ ice = 30 mph  
Serviceability wind speed = 60 mph  
Ice thickness (escalating) = 1.00"  
Exposure = B  
Topographic Category 5 (H = 350')

### Seismic Analysis Criteria:

$S_{DS} = 0.941$   
 $S_{D1} = 0.592$   
 $R = 3.0$   
Site Class 'D' Soils  
 $I = 1.25$

## Tower Analysis Results

The table on the following page summarizes our analysis results. The table expresses the actual stress levels in percentage form relative to what code allows. Stress levels of up to 105% are considered to be acceptable based on the provisions within the existing structures portion of the code. Stress levels higher than 105% require upgrades to the tower or modifications to the loading considered. Refer to the attached computer output for a complete stress summary.

<b>Stress Summary</b>		
Load Combination	Legs	Diagonals
Proposed Antenna Configuration	99%	94%

Please note that our analysis was for the primary structure alone. The connection of the antennas to the mounts, the mounts themselves, and the mount connections to the tower were excluded from our scope of work.

### **Tower Reaction Summary**

The original design loads provided by Rohn are listed in the table below and our calculated reactions are listed beside those for reference. We determined that all of the proposed tower reactions are less than the original design loads primarily due to changes in the building code from the time of the original design to present.

<b>Reaction Summary</b>		
	Rohn Design	Proposed Reactions
Leg Compression	59.3 kips	49.6 kips
Leg Tension	56.8 kips	44.5 kips
Tower Shear	5.1 kips	3.8 kips
Tower OTM	228.8 kip-ft	190.0 kip-ft

Because all of the existing reactions remain less than the design loads, the roof framing and building structural systems should be adequate as originally designed with no further analysis required as allowed by provisions within the International Existing Building Code. Furthermore, our 2022 analysis for the initial Dish collocation included analysis of the building elements and found that the maximum stressed member was at 85% capacity. The proposed reactions have increased negligibly by 2-3%, thus the building framing is adequate by inspection.

### **Conclusions**

We have determined that the existing tower and theater structure below can adequately support the proposed Dish Wireless microwave dish in conformance with applicable code requirements. All tower and roof framing are sufficient for the applied loads and are in conformance with the 2021 IBC and IEBC.

### **Disclaimer**

This structural evaluation was based on the limited documentation that was available to us. Sidesway Engineering did not perform an as-built to verify the accuracy of the building and tower information. We assume the structures were properly constructed and have been maintained to the minimum standards required by code. We assume there to be no known deterioration or damage that would adversely affect structural capacity.

**DESIGNED APPURTENANCE LOADING**

TYPE	ELEVATION	TYPE	ELEVATION
FFVV-65A-R2-V1 w/ 6' Pipe Mount (Dish)	135	6' Pipe Mount (Dish)	135
RF4450T-71A (Dish)	135	5' T-Frame (Dish)	135
RF4451D-70A (Dish)	135	RDIDC-9181-PF-48 w/ 4' Pipe Mount (Dish)	135
6' Pipe Mount (Dish)	135	VHLP2-18 (Dish)	135
5' T-Frame (Dish)	135	EQ4	125
FFVV-65A-R2-V1 w/ 6' Pipe Mount (Dish)	135	DB411-B	119
RF4450T-71A (Dish)	135	4' Standoff Pipe Frame	119
RF4451D-70A (Dish)	135	6812B-2 (Half-Wave) (Mercer Island H.S.)	115 - 95
6' Pipe Mount (Dish)	135	EQ3	105
5' T-Frame (Dish)	135	EQ2	85
FFVV-65A-R2-V1 w/ 6' Pipe Mount (Dish)	135	4' Standoff Pipe Frame	77
RF4450T-71A (Dish)	135	DB411-B	77
RF4451D-70A (Dish)	135	EQ1	65

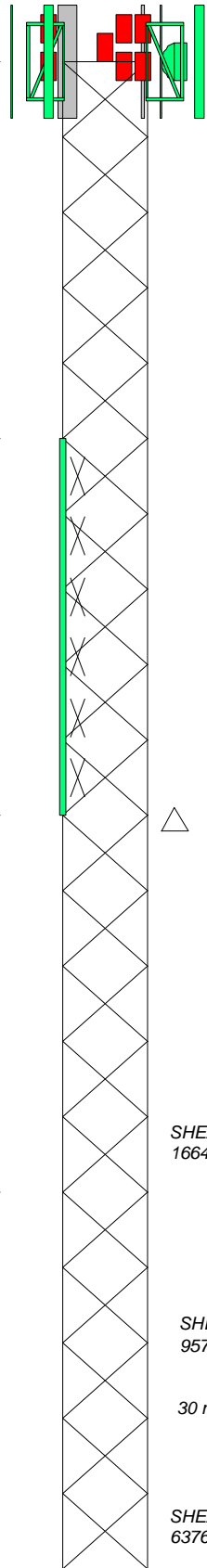
**MATERIAL STRENGTH**

GRADE	Fy	Fu	GRADE	Fy	Fu
A500-50	50 ksi	62 ksi	A36	36 ksi	58 ksi

**TOWER DESIGN NOTES**

1. Tower is located in King County, Washington.
2. Tower designed for Exposure B to the TIA-222-H Standard.
3. Tower designed for a 105 mph basic wind in accordance with the TIA-222-H Standard.
4. Tower is also designed for a 30 mph basic wind with 1.00 in ice. Ice is considered to increase in thickness with height.
5. Deflections are based upon a 60 mph wind.
6. Tower Risk Category III.
7. Topographic Category 5 with Crest Height of 350'
8. TOWER RATING: 98.9%

T1	P2x.154	A500-50	L1 1/2x1 1/2x1/8	A36	20 @ 4	508.0	135.0 ft
T2						491.6	115.0 ft
T3	P2x.218	A500-50	L1 1/2x1 1/2x1/8	A36	N.A.	578.5	95.0 ft
T4	P2.5x.276					748.5	75.0 ft
						2324.7	55.0 ft

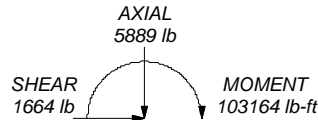


ALL REACTIONS ARE FACTORED

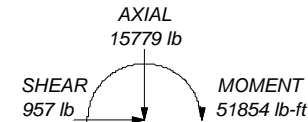
MAX. CORNER REACTIONS AT BASE:

DOWN: 81821 lb  
SHEAR: 3612 lb

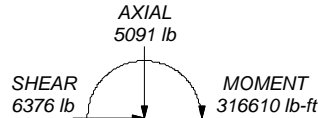
UPLIFT: -74302 lb  
SHEAR: 3425 lb



TORQUE 11 lb-ft  
SEISMIC



TORQUE 504 lb-ft  
30 mph WIND - 1.0000 in ICE



TORQUE 2545 lb-ft  
REACTIONS - 105 mph WIND

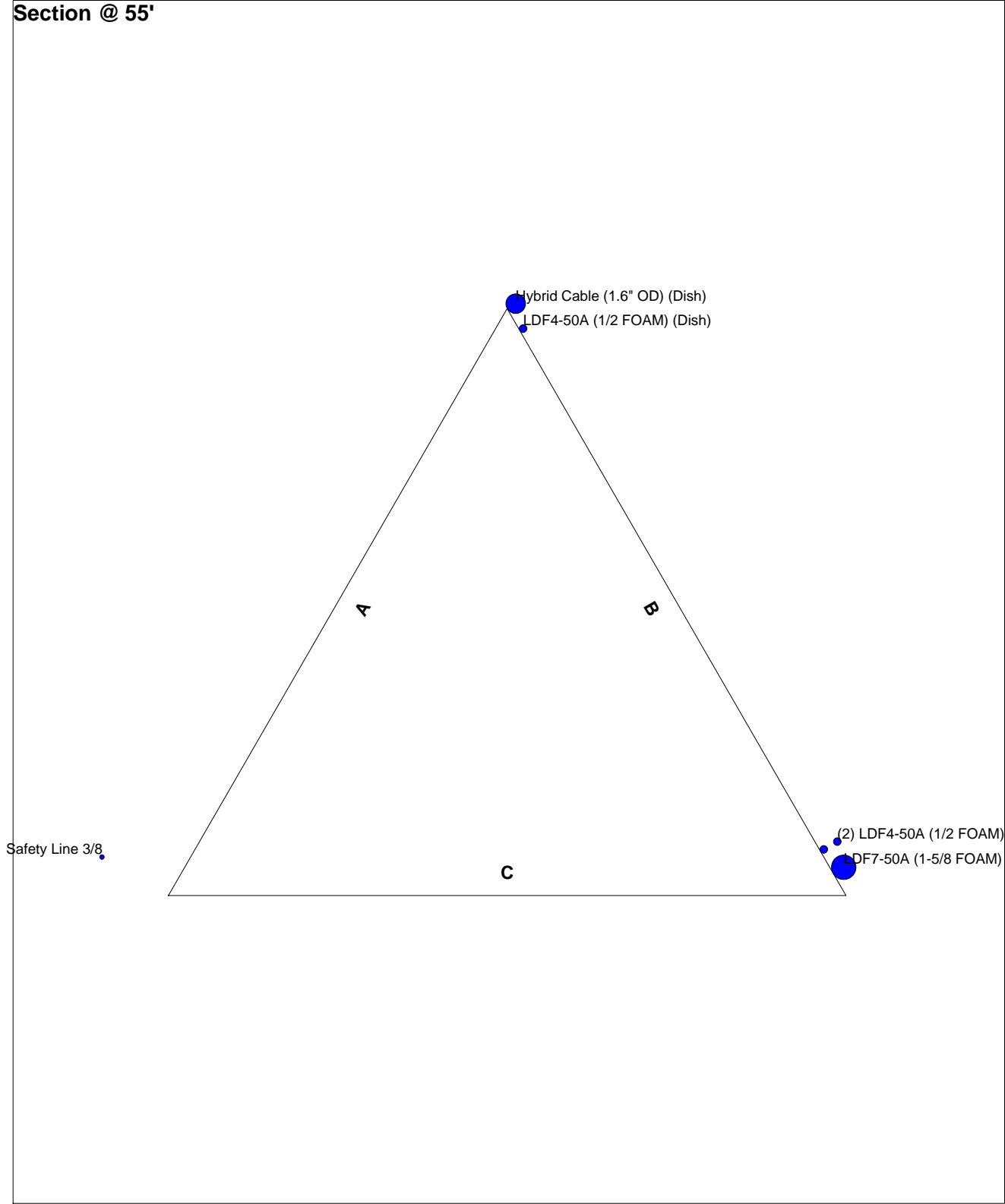

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 Edmonds, WA 98026  
 Phone: 425-673-4160  
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Job: <b>Dish Wireless MW Installation</b>		
Project: <b>21052.05 Mercer Island H.S. 80' Tower</b>		
Client: Day Wireless	Drawn by: CAB	App'd:
Code: TIA-222-H	Date: 06/27/24	Scale: NTS
Path:	Dwg No. E-1	

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Feed Line Plan  
55'

Section @ 55'



Safety Line 3/8'

(Mercer Island H.S.)

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Project: <b>21052.05 Mercer Island H.S. 80' Tower</b>		
Client: Day Wireless	Drawn by: CAB	App'd:
Code: TIA-222-H	Date: 06/27/24	Scale: NTS
Path:	Dwg No. E-7	

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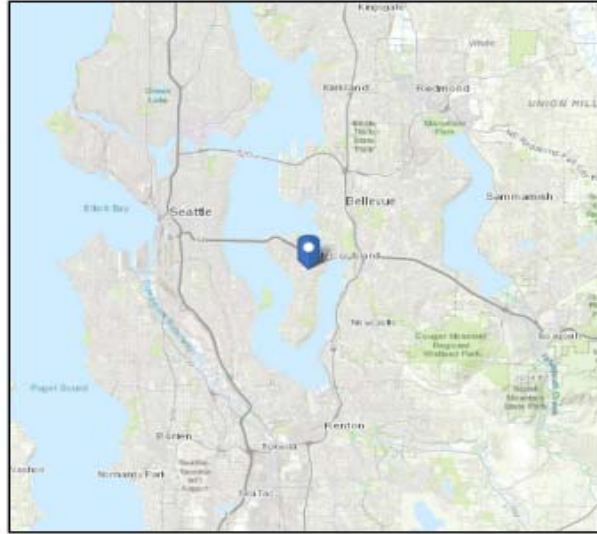


# ASCE 7 Hazards Report

**Address:**  
No Address at This  
Location

**Standard:** ASCE/SEI 7-16  
**Risk Category:** III  
**Soil Class:** D - Stiff Soil

**Elevation:** 347.05 ft (NAVD 88)  
**Latitude:** 47.572362  
**Longitude:** -122.218431



## Wind

### Results:

Wind Speed:	105 Vmph
10-year MRI	67 Vmph
25-year MRI	74 Vmph
50-year MRI	78 Vmph
100-year MRI	83 Vmph

**Data Source:** ASCE/SEI 7-16, Fig. 26.5-1C and Figs. CC.2-1–CC.2-4, and Section 26.5.2  
**Date Accessed:** Thu Jul 15 2021

Value provided is 3-second gust wind speeds at 33 ft above ground for Exposure C Category, based on linear interpolation between contours. Wind speeds are interpolated in accordance with the 7-16 Standard. Wind speeds correspond to approximately a 3% probability of exceedance in 50 years (annual exceedance probability = 0.000588, MRI = 1,700 years).

## Ice

### Results:

Ice Thickness:	1.00 in.
Concurrent Temperature:	25 F
Gust Speed:	30 mph

**Data Source:** Standard ASCE/SEI 7-16, Figs. 10-2 through 10-8  
**Date Accessed:** Thu Jul 15 2021

Ice thicknesses on structures in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

Values provided are equivalent radial ice thicknesses due to freezing rain with concurrent 3-second gust speeds, for a 500-year mean recurrence interval, and temperatures concurrent with ice thicknesses due to freezing rain. Thicknesses for ice accretions caused by other sources shall be obtained from local meteorological studies. Ice thicknesses in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.



<i>Description</i>	Wind & Ice Design Criteria	<i>By</i>	CAB	<i>Project No.</i>
		<i>Date</i>	2/22/22	
<i>Project</i>	Mercer Island HS Tower	<i>Checked</i>		<i>Sheet No.</i>
		<i>Date</i>		



**WIND EXPOSURE CATEGORIES:**

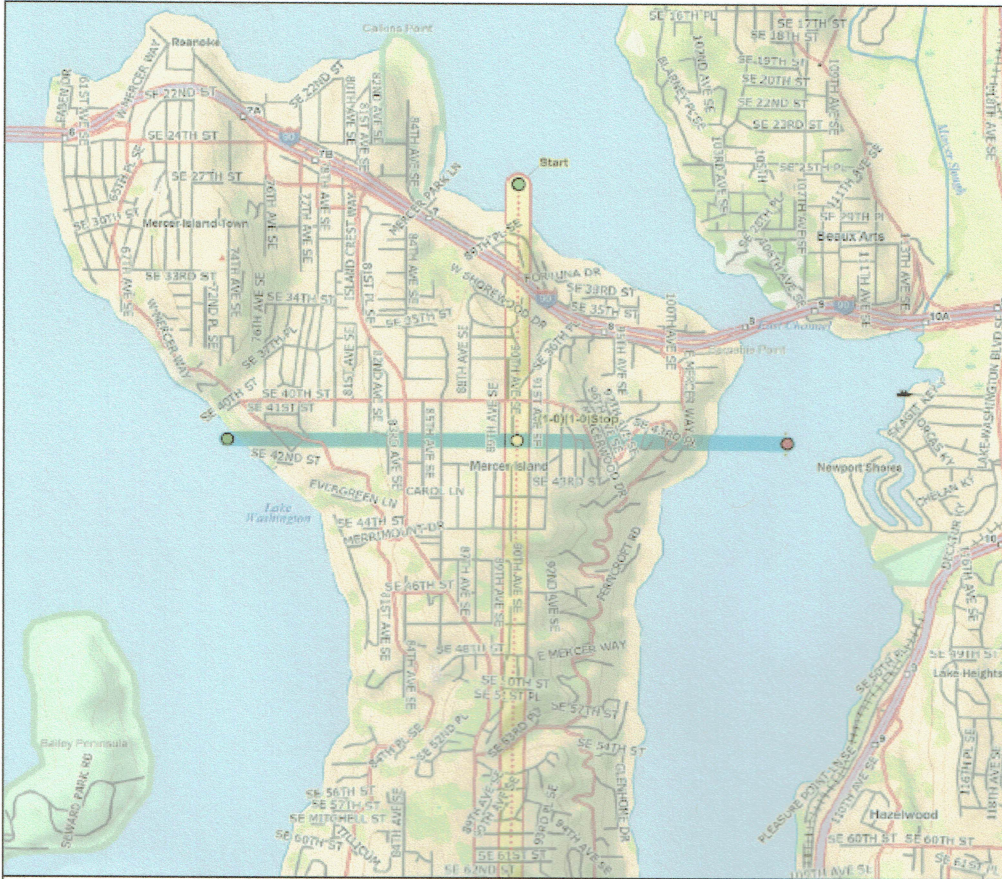
- Wind Exposure Category | Exposure 'C' (1500 feet from Lake)
- | Exposure 'B' (all other areas)

**WIND SPEED-UP (TOPOGRAPHIC EFFECT) -  $K_{z1}$  Factor :**

- $K_{z1}$  Factor |  $K_{z1} = 1.0$
- |  $K_{z1} = 1.3$
- |  $K_{z1} = 1.6$
- |  $K_{z1} = 1.9$

SITE BORDERS  $K_{zT} = 1.3$  &  $K_{zT} = 1.6$   
 $\therefore$  CALCULATE SITE SPECIFIC  $K_{zT}$

DE LORME DeLorme Topo USA® 7.0



BOTH DIRECTIONS ARE FLAT  
 TOPPED HILLS W/ RELIEF  
 ON SIDES OF ISLAND

SEAW RAPID SOLUTION

- HT = 350'
- L<sub>H</sub> = 3960' (3/4 MILE)
- $K_1 = 0.205$
- $K_2 = 1.0$  (@ TOP)
- $K_3 = 0.88$

$K_{zT} = (1 + K_1 K_2 K_3)^2 = 1.40$

RESULTS ARE BETWEEN  
 MAPPED VALUES  $\therefore$  REASONABLE



<i>Description</i>	Topography	By	CAB	Project No.
<i>Project</i>	Mercer Island HS Tower	Date	2/22/22	21052.02
		Checked		Sheet No.
		Date		



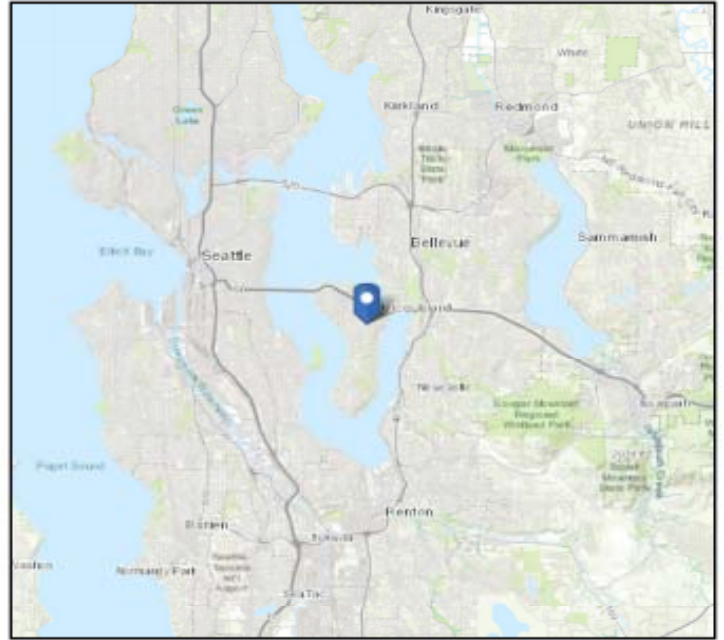


# ASCE 7 Hazards Report

**Address:**  
No Address at This Location

**Standard:** ASCE/SEI 7-16  
**Risk Category:** III  
**Soil Class:** D - Stiff Soil

**Elevation:** 347.05 ft (NAVD 88)  
**Latitude:** 47.572362  
**Longitude:** -122.218431



## Seismic

**Site Soil Class:** D - Stiff Soil

**Results:**

$S_S$ :	1.412	$S_{D1}$ :	N/A
$S_1$ :	0.491	$T_L$ :	6
$F_a$ :	1	PGA :	0.604
$F_v$ :	N/A	PGA <sub>M</sub> :	0.665
$S_{MS}$ :	1.412	$F_{PGA}$ :	1.1
$S_{M1}$ :	N/A	$I_e$ :	1.25
$S_{DS}$ :	0.941	$C_v$ :	1.382

Ground motion hazard analysis may be required. See ASCE/SEI 7-16 Section 11.4.8.

**Data Accessed:** Thu Jul 15 2021

**Date Source:** [USGS Seismic Design Maps](#)



<i>Description</i>	Seismic Design Maps (ASCE 7, USGS)	<i>By</i>	CAB	<i>Project No.</i>	21052.05
		<i>Date</i>	6/27/24		
<i>Project</i>	Mercer Island HS Tower	<i>Checked</i>		<i>Sheet No.</i>	
		<i>Date</i>			

## Self-Supporting Tower Seismic Analysis

### Seismic Parameters:

$S_{DS}$ =	0.941 (ASCE 7, USGS)	$R$ =	3.0 (ASCE Table 15.4-2, Trussed Tower)
$S_{D1}$ =	0.592 (ASCE 7, USGS)	$I$ =	1.25 (ASCE Table 1.5-2, Risk Category III)
$S_1$ =	0.491 (1s Spectral Response)	$f_1$ =	2.824 Hz (Fundamental Frequency)
$T$ =	0.354 (Fundamental Period)	$k_e$ =	1.000 (Distribution Exponent)
$T_s$ =	0.629 ( $S_{D1}/S_{DS}$ )	$K_f$ =	4540 (Constant)
$T_L$ =	16		

### Tower Properties:

Height =	80 ft	$W$ =	4.24 kips
$w_a$ =	4.54 ft	$W_1$ =	4.83 kips
$w_o$ =	4.56 ft	$W_2$ =	1.44 kips

### Seismic Response Coefficient, $C_s$ :

$C_s$ min =	0.044 $S_{DS}I$ = 0.052	$\geq$	0.030
$C_s$ min =	0.8 $S_1I/R$ = 0.164		(If $S_1 > 0.6$ )
$C_s$ =	$S_{DS}I/R$ = 0.392		( $T \leq 1.5T_s$ , ASCE 11.4.8)
$C_s$ max =	$S_{D1}I/TR$ = 1.045		( $T < T_L$ ) (Includes 1.5 increase, ASCE 11.4.8)


### Seismic Base Shear, $V_s$ :

$$V_s = C_s W = 1.663 \text{ kips}$$

### Vertical Distribution of Seismic Forces:

Section	Height (ft)	$w_z$ (lbs)	$w_z h_z^k$	$\frac{w_z h_z^k}{\sum w_z h_z^k}$	$F_{sz}$ (kips)	$\Sigma F_{sz}$ (kips)	$\Sigma M$ (k-ft)
15	80.0	0.0	0.000	0.000	0.000	0.00	0.00
14	80.0	0.0	0.000	0.000	0.000	0.00	0.00
13	80.0	0.0	0.000	0.000	0.000	0.00	0.00
12	80.0	0.0	0.000	0.000	0.000	0.00	0.00
11	80.0	0.0	0.000	0.000	0.000	0.00	0.00
10	80.0	0.0	0.000	0.000	0.000	0.00	0.00
9	80.0	0.0	0.000	0.000	0.000	0.00	0.00
8	80.0	0.0	0.000	0.000	0.000	0.00	0.00
7	80.0	0.0	0.000	0.000	0.000	0.00	0.00
6	80.0	0.0	0.000	0.000	0.000	0.00	0.00
5	80.0	0.0	0.000	0.000	0.000	0.00	0.00
4	70.0	2013.7	140.958	0.687	1.143	1.14	79.98
3	50.0	665.8	33.292	0.162	0.270	1.41	93.47
2	30.0	766.2	22.986	0.112	0.186	1.60	99.06
1	10.0	796.3	7.963	0.039	0.065	1.66	99.70
$\Sigma$		4242.0	205.199		<b>Base Shear, <math>V_s</math> = 1.663 kips</b>		<b>Seismic OTM, <math>M_s</math> = 99.7 kip-ft</b>

**Wind loads govern over seismic loads at each section and for the overall tower.**

	<i>Description</i>	Self Support Tower Seismic Analysis	<i>By</i>	CAB	<i>Project No.</i>
			<i>Date</i>	6/27/24	21052.05
	<i>Project</i>	Mercer Island HS Tower	<i>Checked</i>		<i>Sheet No.</i>
			<i>Date</i>		



<b>Job</b>	Dish Wireless MW Installation	<b>Page</b>	1 of 8
<b>Project</b>	21052.05 Mercer Island H.S. 80' Tower	<b>Date</b>	15:50:11 06/27/24
<b>Client</b>	Day Wireless	<b>Designed by</b>	CAB

## Tower Input Data

This tower is designed using the TIA-222-H standard.

The following design criteria apply:

Tower is located in King County, Washington.

Basic wind speed of 105 mph. Risk Category III.

Exposure Category B.

Rigorous Topographic Factor Procedure for wind speed-up calculations is used.

Topographic Feature: Flat Topped Ridge. Crest Height: 350'.

Slope Distance L: 3960'. Distance from Crest x: 0'.

Nominal ice thickness of 1.00" increased with height.

Ice density of 56 pcf.

A wind speed of 30 mph is used in combination with ice.

Deflections calculated using a wind speed of 60 mph.

A non-linear (P-delta) analysis was used.

Pressures are calculated at each section.

Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

## Tower Section Geometry

Tower Section	Tower Elevation	Assembly Database	Description	Section Width	Number of Sections	Section Length
	ft			ft		ft
T1	135'-115'			4'-1/4"	1	20'
T2	115'-95'			4'-1/4"	1	20'
T3	95'-75'			4'-1/4"	1	20'
T4	75'-55'			4'-23/32"	1	20'

## Tower Section Geometry (cont'd)

Tower Section	Tower Elevation	Diagonal Spacing	Bracing Type	Has K Brace End Panels	Has Horizontals	Top Girt Offset	Bottom Girt Offset
	ft	ft				in	in
T1	135'-115'	4'	X Brace	No	No	0.0000	0.0000
T2	115'-95'	4'	X Brace	No	No	0.0000	0.0000
T3	95'-75'	4'	X Brace	No	No	0.0000	0.0000
T4	75'-55'	4'	X Brace	No	No	0.0000	0.0000

## Tower Section Geometry (cont'd)

Tower Elevation	Leg Type	Leg Size	Leg Grade	Diagonal Type	Diagonal Size	Diagonal Grade
ft						
T1 135'-115'	Pipe	P2x.154	A500-50 (50 ksi)	Single Angle	L1 1/2x1 1/2x1/8	A36 (36 ksi)
T2 115'-95'	Pipe	P2x.154	A500-50 (50 ksi)	Single Angle	L1 1/2x1 1/2x1/8	A36 (36 ksi)
T3 95'-75'	Pipe	P2x.218	A500-50 (50 ksi)	Single Angle	L1 1/2x1 1/2x1/8	A36 (36 ksi)
T4 75'-55'	Pipe	P2.5x.276	A500-50 (50 ksi)	Single Angle	L1 1/2x1 1/2x1/8	A36 (36 ksi)



<b>Job</b> Dish Wireless MW Installation	<b>Page</b> 2 of 8
	<b>Project</b> 21052.05 Mercer Island H.S. 80' Tower
	<b>Date</b> 15:50:11 06/27/24
<b>Client</b> Day Wireless	<b>Designed by</b> CAB

### Tower Section Geometry (cont'd)

Tower Elevation ft	Top Girt Type	Top Girt Size	Top Girt Grade	Bottom Girt Type	Bottom Girt Size	Bottom Girt Grade
T1 135'-115'	Single Angle	L1 1/2x1 1/2x1/8	A36 (36 ksi)	Single Angle		A36 (36 ksi)

### Tower Section Geometry (cont'd)

Tower Elevation ft	Gusset Area (per face) ft <sup>2</sup>	Gusset Thickness in	Gusset Grade	Adjust. Factor A <sub>f</sub>	Adjust. Factor A <sub>r</sub>	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals in	Double Angle Stitch Bolt Spacing Horizontals in	Double Angle Stitch Bolt Spacing Redundants in
T1 135'-115'	1.25	0.1875	A36 (36 ksi)	1	1	1.05	Mid-Pt	Mid-Pt	36.0000
T2 115'-95'	1.25	0.1875	A36 (36 ksi)	1	1	1.05	Mid-Pt	Mid-Pt	36.0000
T3 95'-75'	1.25	0.1875	A36 (36 ksi)	1	1	1.05	Mid-Pt	Mid-Pt	36.0000
T4 75'-55'	1.25	0.1875	A36 (36 ksi)	1	1	1.05	Mid-Pt	Mid-Pt	36.0000

### Tower Section Geometry (cont'd)

Tower Elevation ft	Leg Connection Type	Leg Bolt Size in	Leg No.	Diagonal		Top Girt		Bottom Girt		Mid Girt		Long Horizontal		Short Horizontal	
				Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.
T1 135'-115'	Flange	0.6250	4	0.5000	1	0.5000	1	0.5000	0	0.6250	0	0.5000	0	0.6250	0
T2 115'-95'	Flange	0.6250	4	0.5000	1	0.5000	0	0.5000	0	0.6250	0	0.5000	0	0.6250	1
T3 95'-75'	Flange	0.6250	4	0.5000	1	0.5000	0	0.5000	0	0.6250	0	0.5000	0	0.6250	0
T4 75'-55'	Flange	0.6250	4	0.5000	1	0.5000	0	0.5000	0	0.6250	0	0.5000	0	0.6250	0

### Feed Line/Linear Appurtenances - Entered As Round Or Flat

Description	Face or Leg	Allow Shield	Exclude From Torque Calculation	Component Type	Placement ft	Face Offset in	Lateral Offset (Frac FW)	#	# Per Row	Clear Spacing in	Width or Diameter in	Weight plf
LDF4-50A (1/2 FOAM)	B	No	No	Ar (CaAa)	77' - 55'	0.0000	0.425	2	1	0.6300	0.6300	0.15
LDF4-50A (1/2 FOAM)	B	No	No	Ar (CaAa)	119' - 77'	0.0000	0.425	1	1	0.6300	0.6300	0.15
LDF7-50A (1-5/8 FOAM) (Mercer Island)	B	No	No	Ar (CaAa)	107' - 55'	0.0000	0.4625	1	1	1.9800	1.9800	0.82
Safety Line 3/8	A	No	No	Ar (CaAa)	135' - 55'	6.0000	-0.5	1	1	0.3750	0.3750	0.27
Hybrid Cable (1.6" OD) (Dish)	B	No	No	Ar (CaAa)	135' - 55'	0.0000	-0.5	1	1	1.6000	1.6000	1.00
LDF4-50A (1/2 FOAM) (Dish)	B	No	No	Ar (CaAa)	135' - 55'	0.0000	-0.4625	1	1	0.6300	0.6300	0.15



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### Feed Line/Linear Appurtenances Section Areas

Tower Section	Tower Elevation ft	Face	A <sub>R</sub> ft <sup>2</sup>	A <sub>F</sub> ft <sup>2</sup>	C <sub>AA</sub> In Face ft <sup>2</sup>	C <sub>AA</sub> Out Face ft <sup>2</sup>	Weight lb
T1	135'-115'	A	0.000	0.000	0.750	0.000	5.40
		B	0.000	0.000	4.712	0.000	23.60
		C	0.000	0.000	0.000	0.000	0.00
T2	115'-95'	A	0.000	0.000	0.750	0.000	5.40
		B	0.000	0.000	8.096	0.000	35.84
		C	0.000	0.000	0.000	0.000	0.00
T3	95'-75'	A	0.000	0.000	0.750	0.000	5.40
		B	0.000	0.000	9.806	0.000	42.70
		C	0.000	0.000	0.000	0.000	0.00
T4	75'-55'	A	0.000	0.000	0.750	0.000	5.40
		B	0.000	0.000	10.940	0.000	45.40
		C	0.000	0.000	0.000	0.000	0.00

### Feed Line/Linear Appurtenances Section Areas - With Ice

Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	A <sub>R</sub> ft <sup>2</sup>	A <sub>F</sub> ft <sup>2</sup>	C <sub>AA</sub> In Face ft <sup>2</sup>	C <sub>AA</sub> Out Face ft <sup>2</sup>	Weight lb
T1	135'-115'	A	1.466	0.000	0.000	6.615	0.000	71.36
		B		0.000	0.000	17.614	0.000	223.56
		C		0.000	0.000	0.000	0.000	0.00
T2	115'-95'	A	1.445	0.000	0.000	6.531	0.000	69.69
		B		0.000	0.000	28.909	0.000	362.55
		C		0.000	0.000	0.000	0.000	0.00
T3	95'-75'	A	1.420	0.000	0.000	6.429	0.000	67.65
		B		0.000	0.000	33.167	0.000	414.68
		C		0.000	0.000	0.000	0.000	0.00
T4	75'-55'	A	1.387	0.000	0.000	6.296	0.000	65.08
		B		0.000	0.000	39.492	0.000	465.63
		C		0.000	0.000	0.000	0.000	0.00

### User Defined Loads - Seismic

Description	Elevation ft	Offset From Centroid ft	Azimuth Angle °	E <sub>v</sub> lb	E <sub>hx</sub> lb	E <sub>hz</sub> lb	E <sub>h</sub> lb
EQ1	65'	0'	0.0000	150.00	0.00	0.00	65.00
EQ2	85'	0'	0.0000	144.00	0.00	0.00	186.00
EQ3	105'	0'	0.0000	125.00	0.00	0.00	270.00
EQ4	125'	0'	0.0000	379.00	0.00	0.00	1143.00

### Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	C <sub>AA</sub> Front ft <sup>2</sup>	C <sub>AA</sub> Side ft <sup>2</sup>	Weight lb	
DB411-B	A	From Leg	4.00	0.0000	77'	No Ice	1.50	1.50	25.00
			0'			1/2" Ice	2.70	2.70	32.50

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Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C <sub>AA</sub>		Weight	
			Horz	Vert			Front	Side		
			ft	ft	°	ft	ft <sup>2</sup>	ft <sup>2</sup>	lb	
4' Standoff Pipe Frame	A	From Leg	5'				1" Ice	3.90	3.90	40.00
			2.00		0.0000	77'	No Ice	3.83	4.70	114.60
			0'				1/2" Ice	4.76	5.87	146.76
6812B-2 (Half-Wave) (Mercer Island H.S.)	C	Stand-Off Right	0'				1" Ice	5.51	6.88	186.99
			0.00		0.0000	115' - 95'	No Ice	10.75	10.75	133.00
			4'				1/2" Ice	14.81	14.81	228.54
DB411-B	A	From Leg	0'				1" Ice	18.91	18.91	341.25
			4.00		0.0000	119'	No Ice	1.50	1.50	25.00
			0'				1/2" Ice	2.70	2.70	32.50
4' Standoff Pipe Frame	A	From Leg	5'				1" Ice	3.90	3.90	40.00
			2.00		0.0000	119'	No Ice	3.83	4.70	114.60
			0'				1/2" Ice	4.76	5.87	146.76
FFVV-65A-R2-V1 w/ 6' Pipe Mount (Dish)	A	From Leg	0'				1" Ice	5.51	6.88	186.99
			2.00		0.0000	135'	No Ice	10.59	5.51	110.09
			-2'				1/2" Ice	11.17	6.33	190.04
RF4450T-71A (Dish)	A	From Face	0'				1" Ice	11.71	7.01	277.22
			1.00		0.0000	135'	No Ice	2.06	1.38	94.60
			-2'				1/2" Ice	2.24	1.52	115.26
RF4451D-70A (Dish)	A	From Face	-1'				1" Ice	2.43	1.68	138.87
			1.00		0.0000	135'	No Ice	1.88	1.11	61.30
			-2'				1/2" Ice	2.05	1.25	78.54
6' Pipe Mount (Dish)	A	From Leg	1'				1" Ice	2.22	1.39	98.49
			2.00		0.0000	135'	No Ice	1.43	1.43	21.90
			2'				1/2" Ice	1.92	1.92	32.73
5' T-Frame (Dish)	A	From Leg	0'				1" Ice	2.29	2.29	47.61
			1.00		0.0000	135'	No Ice	3.00	0.75	135.00
			0'				1/2" Ice	3.75	1.00	200.00
FFVV-65A-R2-V1 w/ 6' Pipe Mount (Dish)	B	From Leg	0'				1" Ice	4.50	1.25	265.00
			2.00		0.0000	135'	No Ice	10.59	5.51	110.09
			-2'				1/2" Ice	11.17	6.33	190.04
RF4450T-71A (Dish)	B	From Face	0'				1" Ice	11.71	7.01	277.22
			1.00		0.0000	135'	No Ice	2.06	1.38	94.60
			-2'				1/2" Ice	2.24	1.52	115.26
RF4451D-70A (Dish)	B	From Face	-1'				1" Ice	2.43	1.68	138.87
			1.00		0.0000	135'	No Ice	1.88	1.11	61.30
			-2'				1/2" Ice	2.05	1.25	78.54
6' Pipe Mount (Dish)	B	From Leg	1'				1" Ice	2.22	1.39	98.49
			2.00		0.0000	135'	No Ice	1.43	1.43	21.90
			2'				1/2" Ice	1.92	1.92	32.73
5' T-Frame (Dish)	B	From Leg	0'				1" Ice	2.29	2.29	47.61
			1.00		0.0000	135'	No Ice	3.00	0.75	135.00
			0'				1/2" Ice	3.75	1.00	200.00
FFVV-65A-R2-V1 w/ 6' Pipe Mount (Dish)	C	From Leg	0'				1" Ice	4.50	1.25	265.00
			2.00		0.0000	135'	No Ice	10.59	5.51	110.09
			-2'				1/2" Ice	11.17	6.33	190.04
RF4450T-71A (Dish)	C	From Face	0'				1" Ice	11.71	7.01	277.22
			1.00		0.0000	135'	No Ice	2.06	1.38	94.60
			-2'				1/2" Ice	2.24	1.52	115.26
RF4451D-70A (Dish)	C	From Face	-1'				1" Ice	2.43	1.68	138.87
			1.00		0.0000	135'	No Ice	1.88	1.11	61.30
			-2'				1/2" Ice	2.05	1.25	78.54
6' Pipe Mount (Dish)	C	From Leg	1'				1" Ice	2.22	1.39	98.49
			2.00		0.0000	135'	No Ice	1.43	1.43	21.90
			2'				1/2" Ice	1.92	1.92	32.73
5' T-Frame (Dish)	C	From Leg	0'				1" Ice	2.29	2.29	47.61
			1.00		0.0000	135'	No Ice	3.00	0.75	135.00
			0'				1/2" Ice	3.75	1.00	200.00



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Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C <sub>A</sub> A <sub>A</sub>		Weight
			Horz	Lateral			Front	Side	
			ft	ft	°	ft	ft <sup>2</sup>	ft <sup>2</sup>	lb
RDIDC-9181-PF-48 w/ 4' Pipe Mount (Dish)	A	From Leg	0.50	0.0000	135'	1" Ice	4.50	1.25	265.00
			0'			No Ice	2.83	2.20	36.42
			0'			1/2" Ice	3.17	2.60	66.65
			0'			1" Ice	3.52	3.02	101.07

### Dishes

Description	Face or Leg	Dish Type	Offset Type	Offsets:		Azimuth Adjustment	3 dB Beam Width	Elevation	Outside Diameter	Aperture Area	Weight		
				Horz	Lateral								
			ft	ft	°	°	ft	ft	ft <sup>2</sup>	lb			
VHLP2-18 (Dish)	B	Paraboloid w/Shroud (HP)	From Leg	2.00	-10.0000	135'	2.00	No Ice	3.14	31.00			
				2'							1/2" Ice	3.41	48.50
				0'							1" Ice	3.68	66.00

### Maximum Reactions

Location	Condition	Gov. Load Comb.	Vertical lb	Horizontal, X lb	Horizontal, Z lb
Leg C	Max. Vert	18	81590.90	3000.40	-2057.68
	Max. H <sub>x</sub>	18	81590.90	3000.40	-2057.68
	Max. H <sub>z</sub>	5	-64420.76	-2325.64	1950.30
	Min. Vert	7	-73315.17	-2773.65	1944.38
	Min. H <sub>x</sub>	7	-73315.17	-2773.65	1944.38
	Min. H <sub>z</sub>	18	81590.90	3000.40	-2057.68
Leg B	Max. Vert	10	81691.14	-2993.41	-2091.94
	Max. H <sub>x</sub>	23	-74301.93	2794.90	1979.74
	Max. H <sub>z</sub>	23	-74301.93	2794.90	1979.74
	Min. Vert	23	-74301.93	2794.90	1979.74
	Min. H <sub>x</sub>	10	81691.14	-2993.41	-2091.94
	Min. H <sub>z</sub>	10	81691.14	-2993.41	-2091.94
Leg A	Max. Vert	2	81820.79	-47.19	3612.19
	Max. H <sub>x</sub>	20	2780.91	836.52	-10.19
	Max. H <sub>z</sub>	2	81820.79	-47.19	3612.19
	Min. Vert	15	-72358.86	41.09	-3358.50
	Min. H <sub>x</sub>	8	1916.41	-843.91	-35.67
	Min. H <sub>z</sub>	15	-72358.86	41.09	-3358.50

### Maximum Tower Deflections - Service Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
T1	135 - 115	4.220	39	0.3780	0.0546
T2	115 - 95	2.650	39	0.3574	0.0508
T3	95 - 75	1.282	39	0.2721	0.0386
T4	75 - 55	0.357	39	0.1426	0.0229

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### Maximum Tower Deflections - Design Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
T1	135 - 115	12.746	2	1.1402	0.1675
T2	115 - 95	8.011	2	1.0778	0.1560
T3	95 - 75	3.879	2	0.8225	0.1186
T4	75 - 55	1.081	2	0.4311	0.0704

### Bolt Design Data

Section No.	Elevation ft	Component Type	Bolt Grade	Bolt Size in	Number Of Bolts	Maximum Load per Bolt lb	Allowable Load per Bolt lb	Ratio Load Allowable	Allowable Ratio	Criteria
T1	135	Leg	A325N	0.6250	4	1993.08	20340.10	0.098 ✓	1	Bolt Tension
		Diagonal	A325N	0.5000	1	1261.10	3126.56	0.403 ✓	1	Member Block Shear
		Top Girt	A325N	0.5000	1	250.76	3126.56	0.080 ✓	1	Member Block Shear
T2	115	Leg	A325N	0.6250	4	5875.96	20340.10	0.289 ✓	1	Bolt Tension
		Diagonal	A325N	0.5000	1	1945.75	3126.56	0.622 ✓	1	Member Block Shear
T3	95	Leg	A325N	0.6250	4	11147.60	20340.10	0.548 ✓	1	Bolt Tension
		Diagonal	A325N	0.5000	1	2381.40	3126.56	0.762 ✓	1	Member Block Shear
T4	75	Leg	A325N	0.6250	4	17745.90	20340.10	0.872 ✓	1	Bolt Tension
		Diagonal	A325N	0.5000	1	2947.65	3126.56	0.943 ✓	1	Member Block Shear

### Leg Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> lb	φP <sub>n</sub> lb	Ratio P <sub>u</sub> / φP <sub>n</sub>
T1	135 - 115	P2x.154	20'	4'	61.0 K=1.00	1.0745	-9599.30	36842.20	0.261 <sup>1</sup> ✓
T2	115 - 95	P2x.154	20'	4'	61.0 K=1.00	1.0745	-26299.50	36842.20	0.714 <sup>1</sup> ✓
T3	95 - 75	P2x.218	20'	4'	62.6 K=1.00	1.4773	-49343.00	49904.80	0.989 <sup>1</sup> ✓
T4	75 - 55	P2.5x.276	20'	4'	51.9 K=1.00	2.2535	-78011.80	83252.00	0.937 <sup>1</sup> ✓

### Diagonal Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> lb	φP <sub>n</sub> lb	Ratio P <sub>u</sub> / φP <sub>n</sub>
T1	135 - 115	L1 1/2x1 1/2x1/8	6'15/32"	2'9-3/8"	114.5 K=1.02	0.3594	-1273.81	7601.18	0.168 <sup>1</sup> ✓



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Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> lb	φP <sub>n</sub> lb	Ratio $\frac{P_u}{\phi P_n}$
T2	115 - 95	L1 1/2x1 1/2x1/8	6'15/32"	2'9-3/8"	114.5 K=1.02	0.3594	-1988.23	7601.18	0.262 <sup>1</sup> ✓
T3	95 - 75	L1 1/2x1 1/2x1/8	6'23/32"	2'9-19/32"	115.1 K=1.01	0.3594	-2475.71	7552.04	0.328 <sup>1</sup> ✓
T4	75 - 55	L1 1/2x1 1/2x1/8	6'27/32"	2'9-1/4"	114.2 K=1.02	0.3594	-3331.04	7633.82	0.436 <sup>1</sup> ✓

### Top Girt Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> lb	φP <sub>n</sub> lb	Ratio $\frac{P_u}{\phi P_n}$
T1	135 - 115	L1 1/2x1 1/2x1/8	4'6-1/4"	4'1-5/16"	166.7 K=1.00	0.3594	-249.85	3701.39	0.068 <sup>1</sup> ✓

### Leg Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> lb	φP <sub>n</sub> lb	Ratio $\frac{P_u}{\phi P_n}$
T1	135 - 115	P2x.154	20'	4'	61.0	1.0745	7972.33	48353.90	0.165 <sup>1</sup> ✓
T2	115 - 95	P2x.154	20'	4'	61.0	1.0745	23503.80	48353.90	0.486 <sup>1</sup> ✓
T3	95 - 75	P2x.218	20'	4'	62.6	1.4773	44590.50	66476.60	0.671 <sup>1</sup> ✓
T4	75 - 55	P2.5x.276	20'	4'	51.9	2.2535	70983.60	101409.00	0.700 <sup>1</sup> ✓

### Diagonal Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> lb	φP <sub>n</sub> lb	Ratio $\frac{P_u}{\phi P_n}$
T1	135 - 115	L1 1/2x1 1/2x1/8	6'15/32"	2'9-3/8"	74.5	0.2109	1261.10	9175.78	0.137 <sup>1</sup> ✓
T2	115 - 95	L1 1/2x1 1/2x1/8	6'15/32"	2'9-3/8"	74.5	0.2109	1945.75	9175.78	0.212 <sup>1</sup> ✓
T3	95 - 75	L1 1/2x1 1/2x1/8	6'23/32"	2'9-19/32"	74.9	0.2109	2381.40	9175.78	0.260 <sup>1</sup> ✓
T4	75 - 55	L1 1/2x1 1/2x1/8	6'27/32"	2'9-1/4"	74.2	0.2109	2947.65	9175.78	0.321 <sup>1</sup> ✓

### Top Girt Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> lb	φP <sub>n</sub> lb	Ratio $\frac{P_u}{\phi P_n}$
T1	135 - 115	L1 1/2x1 1/2x1/8	4'6-1/4"	4'1-5/16"	111.5	0.2109	250.76	9175.78	0.027 <sup>1</sup> ✓

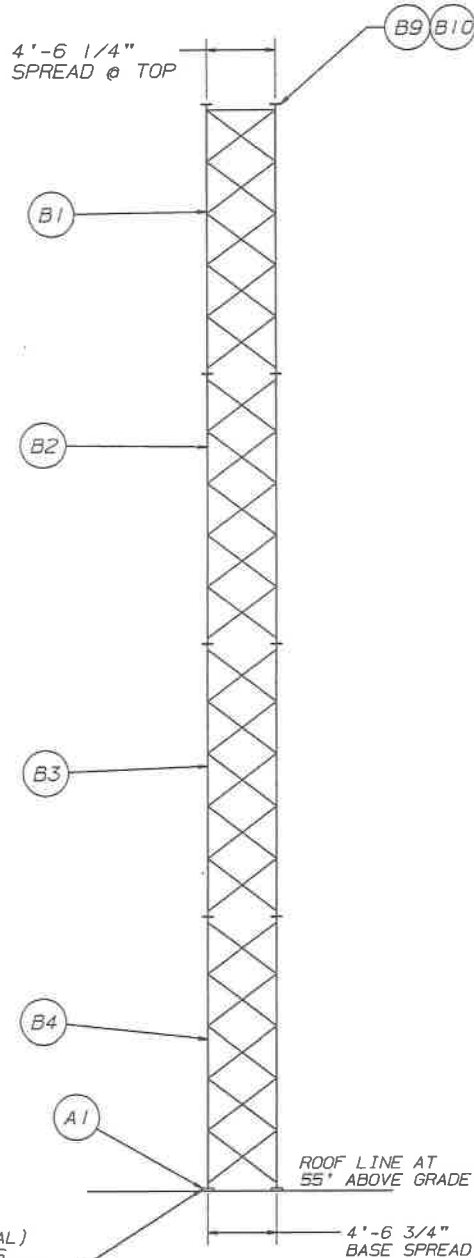


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### Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P lb	$\phi P_{allow}$ lb	% Capacity	Pass Fail	
T1	135 - 115	Leg	P2x.154	3	-9599.30	36842.20	26.1	Pass	
		Diagonal	L1 1/2x1 1/2x1/8	9	-1273.81	7601.18	16.8	Pass	
		Top Girt	L1 1/2x1 1/2x1/8	6	-249.85	3701.39	40.3 (b) 6.8	Pass	
T2	115 - 95	Leg	P2x.154	39	-26299.50	36842.20	71.4	Pass	
		Diagonal	L1 1/2x1 1/2x1/8	45	-1988.23	7601.18	26.2	Pass	
T3	95 - 75	Leg	P2x.218	72	-49343.00	49904.80	62.2 (b) 98.9	Pass	
		Diagonal	L1 1/2x1 1/2x1/8	78	-2475.71	7552.04	32.8	Pass	
T4	75 - 55	Leg	P2.5x.276	105	-78011.80	83252.00	76.2 (b) 93.7	Pass	
		Diagonal	L1 1/2x1 1/2x1/8	108	-3331.04	7633.82	43.6	Pass	
							94.3 (b)		
							Summary		
							Leg (T3)	98.9	Pass
							Diagonal (T4)	94.3	Pass
							Top Girt (T1)	8.0	Pass
							Bolt Checks	94.3	Pass
							<b>RATING =</b>	<b>98.9</b>	<b>Pass</b>

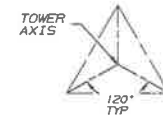
TOWER HT. =80'



4 A-BOLTS (12 TOTAL)  
SUPPLIED BY OTHERS  
(MUST BE A325 QUALITY)  
5/8" DIA. X LENGTH AS  
REQUIRED (SEE NOTE #26)

TOWER DESIGN LOADING				
DESIGN WIND LOAD PER ANSI/TIA/EIA-222-F 1996, 80 MPH BASIC WIND SPEED (1/2" RADIAL ICE LOAD).				
THIS TOWER IS DESIGNED TO SUPPORT THE FOLLOWING LOADS:				
ELEVATION (FT.)	ANTENNA TYPE	E. P. A. (SF)		LINE SIZE
		NO ICE	WITH ICE	
TOP	(2) UHF/VHF ANTENNAS W/ STUB MOUNTS	8.0	12.0	(2)
		TOTAL	TOTAL	7/8"
75	(1) UHF/VHF ANTENNAS W/ (1) 3' SIDE ARM	7.8	10.6	(1)
		TOTAL	TOTAL	7/8"
60	(1) UHF/VHF ANTENNA LEG MOUNTED	3.0	4.5	(1)
		TOTAL	TOTAL	7/8"

FOR BILL OF MATERIALS SEE DWG. CM971875-1  
FOR GENERAL NOTES SEE DWG. CT971875,1-2



TOWER CONFIGURATION  
N. T. S.

TOWER SITE: MERCER ISLAND, WA  
KING COUNTY

TOWER REACTIONS	
COMPRESSION	59.3 KIPS
TENSION	56.8 KIPS
TOTAL SHEAR	5.1 KIPS
O. T. M.	228.8 FT.-KIPS

No.	Revision Description	Date	Rev By	Ckd By	Appd By
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					<b>ROHN</b>
Scale:	NONE	By	LLK	Date	11/14/97
Drawn:	LLK	Date	12-16-97	Title:	
Checked:	JAM	Date	12-17-97	80' SSV (ROOF MOUNTED) TOWER ASSEMBLY FOR BERSCHAUER PHILLIPS CONSTRUCTION CO.	
App. Eng.:	JTC	Date	12-17-97	ENG. FILE 35832PM001	
App. Sales:	JAM	Date	12-17-97	DRAWING NO.: C971875	